Modified Level II Streambed-Scour Analysis for Structure I-465-165-4442 Crossing Lick Creek in Marion County, Indiana

By BRET A. ROBINSON, DAVID C. VOELKER, and ROBERT L. MILLER

Prepared in cooperation with the INDIANA DEPARTMENT OF TRANSPORTATION

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# U.S. DEPARTMENT OF THE INTERIOR BRUCE BABBITT, Secretary

U.S. GEOLOGICAL SURVEY Gordon P. Eaton, Director

For additional information, write to: District Chief U.S. Geological Survey Water Resources Division 5957 Lakeside Boulevard Indianapolis, IN 46278-1996 Copies of this report can be purchased from: U.S. Geological Survey Branch of Information Services Box 25286 Federal Center Denver, CO 80225

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### CONVERSION FACTORS AND ABBREVIATIONS

Multiply	Ву	To obtain
inch (in.)	25.4	millimeter
foot (ft)	0.3048	meter
square foot (ft²)	929.0	square centimeter
feet per second (ft/s)	0.3048	meters per second
cubic foot per second (ft <sup>3</sup> /s)	0.02832	cubic meter per second
mile (mi)	1.609	kilometer
square mile (mi <sup>2</sup> )	2.590	square kilometer

#### Abbreviations used in this report:

$D_{50}$	median diameter of bed material
Q100	100-year discharge
FEMA	Federal Emergency Management Agency
HEC	Hydraulic Engineering Circular
IDNR	Indiana Department of Natural Resources
INDOT	Indiana Department of Transportation
USGS	U. S. Geological Survey
WSPRO	Water Surface PROfile model

# Modified Level II Streambed-Scour Analysis for Structure I-465-165-4442 Crossing Lick Creek in Marion County, Indiana

By Bret A. Robinson, David C. Voelker, and Robert L. Miller

#### **ABSTRACT**

Level II scour evaluations follow a process in which hydrologic, hydraulic, and sediment-transport data are evaluated to calculate the depth of scour that may result when a given discharge is routed through a bridge opening. The results of the modified Level II analysis for structure I-465-165-4442 in Indianapolis where Carson Avenue crosses Lick Creek are presented. The site is in the city of Indianapolis in the southeastern part of Marion County. Scour depths were computed with the Water Surface PROfile model, version V050196, which incorporates the scour-calculation procedures outlined in Hydraulic Engineering Circular No. 18. Total scour depths at the piers were approximately 8.4 feet for the modeled discharge of 6,890 cubic feet per second and approximately 10.5 feet for the modeled discharge of 9,640 cubic feet per second.

#### INTRODUCTION

The U.S. Geological Survey (USGS), in cooperation with the Indiana Department of Transportation (INDOT), is conducting Level II scour analyses at a number of bridges throughout Indiana. This report describes the methods applied and the modeling results for bridge I-465-165-4442.

#### **Background and Scope**

Level I scour assessment is a process where a large number of bridges are studied as a group. Assessments usually are made by evaluating a combination of geomorphic, hydrologic, and bridge-characteristic data. The results help investigators determine which bridges appear to be most likely to experience streambed-scour problems and which bridges appear to be relatively immune to problems brought on by streambed scour (for example, bridges built on bedrock).

When applied correctly, Level I scour assessments provide an investigator with information to identify those bridges that appear to be relatively safe and those bridges that fall into higher risk categories.

Level II scour evaluations describe the process for an investigator to apply a model to a bridge site and calculate the potential depth of scour that may result from a given flood event. Level II analyses involve the application of basic hydrologic, hydraulic, and sediment-transport engineering concepts and may include an evaluation of flood history, channel hydraulic conditions (for example, water-surface profile analysis), and basic sediment-transport analyses such as scour calculations (Lagasse and others, 1995).

The methods and model outlined in Hydraulic Engineering Circular (HEC) No. 18 (Richardson and Davis, 1995) formulate the basis for Level II scour evaluations. Methods used in this study for Level II scour evaluations are a modification of the HEC-18 standards. These modifications were made to comply with the methodology requested by INDOT (Merril Dougherty, Indiana Department of Transportation, oral commun., 1996). Descriptions of the specific modifications are given in the "Evaluation Methods" section of this report.

This report presents the methods followed for modeling, special considerations for this study site, and the input for and the output from the Water Surface PROfile (WSPRO) model.

#### **Site Description**

The study site is located in the city of Indianapolis in the southeastern part of Marion County. The drainage area for the site is approximately 16.1 mi<sup>2</sup> (Merril Dougherty, Indiana Department of Transportation, written commun., 1996). The predominant land use in the basin is urban; in the immediate vicinity of the bridge, the land is predominantly urban.

Within the immediate vicinity of the bridge, Lick Creek has a channel-bed slope of approximately 0.0011 ft/ft. The channel-bed material is gravel, silt-clay, and sand; the channel banks consist of gravelly sandy silt-clay and concrete. At the time of the Level I site visit on July 24, 1995, the banks were observed to have 0 to 25 percent woody vegetative cover; the field report noted that the banks were experiencing some fluvial erosion.

The Carson Avenue crossing of Lick Creek and Interstate 465 is a 417-ft-long, multi-lane bridge consisting of seven spans supported by concrete and steel piers and sloping concrete spill-through abutments. Additional details describing conditions at the site are included in the Level I data base (Hopkins and Robinson, unpub. data, 1997). Photographs of the site, taken at the time of the Level I site visit, are archived at the USGS office in Indianapolis.

#### **EVALUATION METHODS**

The methods described in this section apply to a number of bridge sites in Indiana being evaluated for scour and outline the procedures requested by INDOT for these modified Level II scour analyses. The principal modification requested by INDOT was that the input data to the model come from or be estimated from existing data sources; no additional field data were collected. Actual methods used in the scour evaluation at this particular bridge site use the most applicable method possible, given the data available.

In Indiana, flood discharges are coordinated by agreement among State and Federal agencies. At sites where flood discharges officially are coordinated among State and Federal agencies in Indiana, the coordinated 100-year discharge (Q100) was modeled. INDOT also provided an additional flood discharge for these coordinated sites in excess of the Q100 to be modeled.

If a flood discharge was not coordinated, the USGS examined Federal Emergency Management Agency (FEMA) studies for Q100 determinations. Where FEMA studies did not produce a Q100, the USGS contacted IDNR for an estimated Q100 in the vicinity of the site being studied. If IDNR did not have a Q100, data from nearby USGS streamflow-gaging stations were analyzed with nearby and similar drainage basins that have been coordinated. At sites having no coordinated discharge data, the two discharges used in the model were 1) the approximated Q100 and 2) a discharge equal to 1.7 times the approximated Q100.

Most of the cross-section and bridge-opening geometry data were taken from the bridge plans (Indiana State Highway Commission, 1962, 1981) provided by INDOT. Bridge plans are presumed to be representative of current conditions at the site. To determine the cross-section geometry, a line was drawn on the bridge plans parallel to the bridge stationing and approximately one bridge width from the bridge. For sites where the bridge plans did not extend far enough laterally for collection of all cross-section data required for WSPRO model analysis, additional data were collected from 7.5-minute topographic maps.

The roadway and embankment profile was taken from the bridge and highway plans for those sites where roadway overtopping was expected. The INDOT bridge plans and 7.5-minute topographic maps were used as a guide, based on the water-surface elevations calculated by the WSPRO model, to determine if roadway overtopping might occur.

Roughness values (*n*-values) for the main channel were estimated by viewing photographs archived from the Level I scour assessments. The *n*-values for the overbanks were assigned on the basis of the surface-cover data summarized in the Level I data base (Hopkins and Robinson, unpub. data, 1997). From those data, the following roughness values were assigned to the surface-cover categories: urban—0.050, suburban—0.035, row crop—0.045, pasture—0.035, brush—0.120, forest—0.100, and wetland (any area covered by standing water)—0.100. The *n*-values for the overbanks were adjusted if the Level I photographs provided sufficient detail to warrant an adjustment.

WSPRO version V050196 was used to model flow through the study site. Starting water-surface elevation was obtained with a slope-conveyance computation. The channel-bed slope in the immediate vicinity of the bridge was estimated from the 7.5-minute topographic map and was used as the slope of the energy grade line for this computation.

WSPRO version V050196 includes a field that allows the input of up to four scour-adjustment factors (K1 to K4). For this modeling, the default value for K4 (bed armoring) was chosen. For scour-adjustment factors K1 and K2 (pier-nose shape and angle of attack, respectively), input values were determined by evaluating the data archived in the Level I data base (Hopkins and Robinson, unpub. data, 1997). For the K3 factor (bed forms), a value of 1.1 was applied in all cases.

In some cases, piers set on the overbanks are constructed with footings that are higher in elevation than pier footings in the main channel. In these situations, if the channel position changes, the piers that were initially constructed on the overbank may become part of the main channel. Therefore, to evaluate total potential scour, the model results obtained for contraction scour and deepest local scour in the main channel were added and applied to all piers in the bridge opening. This methodology allowed for an evaluation of potential undermining of pier supports in the event that future channel movement placed overbank piers in the main channel.

Where bridge pairs have a continuous abutment or fill between the bridges that does not allow expansion of flow, the bridge pair was modeled as one bridge. Sites with discontinuous abutments, allowing expansion between the bridges, were modeled as two separate bridges. In those cases, a valley cross section was measured between the bridges and used as the approach section for the downstream bridge and as the exit section for the upstream bridge.

At sites with no embankment to function as a weir or at sites where the tailwater drowns out the embankment, a composite bridge and road section was used to compute flow. Those sites were computed with friction-loss equations rather than with a bridge routine.

Total scour is taken as the sum of local scour plus contraction scour. If the model predicted negative contraction scour (aggradation), the contraction-scour value was assumed to be zero in determining the total scour depth (table 1). This assumption was made so that a negative contraction scour would not mask the potentially detrimental effects of local scour at a pier. No abutment scour evaluations were made in this study.

Table 1. Cumulative scour depths for the modeled discharges at structure I-465-165-4442 crossing Lick Creek in Marion County, Indiana [--, no value]

Pier number <sup>1</sup>	Stationing from bridge plans <sup>2</sup>	Initial bed- elevation at pier (feet)	Main- channel contrac- tion scour depth (feet)	Local scour depth (feet)	Worst- case total- scour depth <sup>3</sup> (feet)	Bottom elevation of pier (feet)	Worst- case bed elevation after scour <sup>4</sup> (feet)
		Modeled	discharge <sup>5</sup> is 6,8	90 cubic feet p	er second		
1	16+81	736	2.6	5.8	8.4	728.5	726.3
2	17+61	740	2.6	5.8	8.4	728.6	726.3
		Modeled	discharge is 9,64	10 cubic feet p	er second		
1	16+81	736	4.2	6.3	10.5	728.5	724.2
2	17+61	740	4.2	6.3	10.5	728.6	724.2

<sup>&</sup>lt;sup>1</sup>Pier numbers were assigned from left to right as shown on the bridge plans.

<sup>&</sup>lt;sup>2</sup>Stationing is the center line of the pier as determined from the bridge plans. Stationing from bridge plan, 16+81, represents a point 1,681 feet from an arbitrary starting location referenced on the bridge plans.

<sup>&</sup>lt;sup>3</sup>Worst-case total-scour depths are generated by summing the calculated contraction-scour depth with the worst case of local scour.

<sup>&</sup>lt;sup>4</sup>Worst-case bed elevation is computed by subtracting the worst-case total-scour depth from the lowest initial bed elevation in the bridge opening (734.7 feet).

<sup>&</sup>lt;sup>5</sup>Coordinated discharge.

#### SPECIAL CONSIDERATIONS

Model runs indicate the water-surface elevation at the bridge is lower than the low-steel elevation for the modeled discharges. Therefore, there should be no pressure flow through the bridge opening for the discharges modeled.

#### **RESULTS**

Scour depths were computed with a version of WSPRO (Larry Arneson, Federal Highway Administration, written commun., 1996) modified from Shearman (1990). This version of WSPRO includes scour calculations in the model output. Scour depths were calculated assuming an infinite depth of material that could erode and a homogeneous particle-size distribution. The results of the scour analysis are presented in table 1; a complete input file and output results are presented in the appendix.

#### **REFERENCES**

- Hoggatt, R.E., 1975, Drainage areas of Indiana streams: U.S. Geological Survey, Water Resources Division, 231 p.
- Indiana State Highway Commission, 1962, Bridge plans Interstate Route 465: Bridge File I-465-165-4442.
- Indiana State Highway Commission, 1981, Bridge plans Interstate Route 465: Bridge File I-465-165-4442.
- Lagasse, P.F.; Schall, J.D.; Johnson, F.; Richardson, E.V.; and Chang, F., 1995, Stream stability at highway structures (2d ed.): Federal Highway Administration, Hydraulic Engineering Circular No. 20, Publication FHWA-IP-90-014, 144 p.
- Richardson, E.V., and Davis, S.R., 1995, Evaluating scour at bridges (3d ed.): Federal Highway Administration, Hydraulic Engineering Circular No. 18, Publication FHWA-IP-90-017, 204 p.
- Shearman, J.O., 1990, User's manual for WSPRO, a computer model for water-surface profile computations: Federal Highway Administration Publication FHWA-IP-89-027, 177 p.

**APPENDIX** 

#### WSPRO INPUT FILE

```
Т1
          Carson Ave Over Lick Creek and I-465 I-465-165-4442
Т2
          County: Marion
                                               Quad: Beech Grove 124 B
          4-10-97
Т3
                                               Bret A. Robinson
SI
          0
          6980
Q
Q
          9640
SK
          .0011 .0011
XS
     EXIT 0 0
GR
          937 750 1054 740 1677 740 1694 740 1706 735 1730 734.5
GR
          1756 735 1770 740 1810 740 1845 750 1906 760
N
          .100 .035
          1692
SA
XS
     FULLV 150 0
          937 750 1054 740 1677 740 1694 740 1706 735 1730 734.5
GR
          1756 735 1770 740 1810 740 1845 750 1906 760
GR
N
          .100 .035
          1692
SA
BR
     BRDGE 150 760 0
          1628 0760.2 1628 0759.1 1630 0759.0 1630 0758.4 1633 0758.3
GR
                                                1754 0734.7
          1672 0739.8 1691 0739.7 1703 0734.7
GR
                                                             1765 0739.8
GR
          1795 0739.8 1808 0747.0 1819 0747.9
                                               1880 0749.8
                                                            1894 0749.0
          1933 0749.0 1951 0750.2 1991 0748.7
                                                2008 0747.9
                                                             2045 0765.2
GR
GR
          2047 0765.2 2048 0765.4 2049 0765.4 2049 0765.7
                                                             2038 0765.9
GR
          2024 0766.0 2000 0766.3 1974 0766.3 1942 0766.4 1916 0766.3
          1880 0766.1 1835 0765.5 1814 0765.3 1783 0764.7 1752 0764.1
GR
GR
          1718 0763.1 1682 0762.1 1647 0760.9 1630 0760.2 1628 0760.2
          .034
N
          736.2 2 1
PD
          740
               2 2
PD
          740
               4 3
PD
          747
               4 4
PD
               6 5
PD
         747
          3 110 2 758.3
CD
          LXBr RXBr LXApp RXApp * TPierW
DC 0 BRDGE 1692 1766 1695 1770 * 6
         LPierEdge RPierEdge PierWdth * * K1 K2 K3(1.1)
          1628 2049 2 * * 1 1 1.1
DP
DP
          1628 2049 2 * * 1 1 1.1
XS
    APPR 410 0
         968 760 1024 755 1114 750 1230 745 1675 740 1695 740 1706 735
GR
         1730 734.5 1755 735 1769 740 1799 740 1804 750 1862 760
GR
N
          .100 .035
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SA
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T1 CARSON AVE OVER T2 COUNTY: MARION T3 4-10-97 SI 0 Q 6980 Q 9640		AND I-465		OVE 124 B
*** Processing Flow Da	ta; Placing	Information	into Sequence	1 ***
SK .0011 .0011				
**************************************	inistration ter-Surface : English / 0	- U.S.O Profile Com Output Unit	Seological Surv mputations. s: English	ey
CARSON AVE OVER LI COUNTY: MARION 4-10-97	CK CREEK AND	I-465 I-4 QUAD: BE BRET	65-165-4442 ECH GROVE 124 E A. ROBINSON	
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XS EXIT 0 0 GR 937 750 1054 7 GR 1756 735 1770 N .100 .035 SA 1692				0 734.5
*** Completed Reading  *** Storing X-Section D				
*** Data Su SRD Location: 0. Valley Slope: .00000 Energy Loss Coefficients	Averaging (	ion Skew: Conveyance	.0 Error Co	ean.
	coordinates		77	17
Х У	X	Y	X	Y
937.000 750.000	1054.000	740.000	1677.000	740.000
1694.000 740.000 1756.000 735.000	1706.000 1770.000	735.000 7 <b>4</b> 0.000	1730.000 1810.000	734.500 740.000
1845.000 750.000	1906.000	760.000		

Maximum X-S Minimum Y-E	tation: tation: levation: levation: Rough	Coefficien	ssociated Y- ssociated Y- ssociated X- ssociated X- 2 SubAreas Horizonta t Breakpoir	Elevation: Elevation: Station: Station:	760.000 ) 1730.000 )
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*** SRD Location Valley Slope Energy Loss (	: 150. : .00000	• -	ion Skew: Conveyance B	.0 Error	
x	X, Y-	coordinates X	(11 pairs) Y	х	Y
937.000 1694.000 1756.000 1845.000	750.000 740.000 735.000 750.000	1054.000 1706.000 1770.000 1906.000	740.000 735.000 740.000 760.000	1677.000 1730.000 1810.000	734.500

```
Minimum and Maximum X, Y-coordinates
   Minimum X-Station: 937.000 (associated Y-Elevation: 750.000)
   Maximum X-Station:
                    1906.000 (associated Y-Elevation: 760.000)
   Minimum Y-Elevation: 734.500 (associated X-Station: 1730.000)
   Maximum Y-Elevation: 760.000 (associated X-Station: 1906.000)
                  Roughness Data ( 2 SubAreas )
                        Roughness Horizontal
                SubArea Coefficient Breakpoint
                        -----
                           .100
                           - - -
                                   1692.000
                           .035
                   2
                       ......
              Finished Processing Header Record FULLV
         *----*
    Federal Highway Administration - U. S. Geological Survey
            Model for Water-Surface Profile Computations.
           Input Units: English / Output Units: English
    *----*
       CARSON AVE OVER LICK CREEK AND I-465 I-465-165-4442
    COUNTY: MARION
                                  QUAD: BEECH GROVE 124 B
       4-10-97
                                     BRET A. ROBINSON
         *----*
               Starting To Process Header Record BRDGE
         *----*
     BRDGE 150 760 0
 BR
 GR
         1628 0760.2 1628 0759.1 1630 0759.0 1630 0758.4 1633 0758.3
         1672 0739.8 1691 0739.7 1703 0734.7 1754 0734.7 1765 0739.8
 GR
         1795 0739.8 1808 0747.0 1819 0747.9 1880 0749.8 1894 0749.0
 GR
         1933 0749.0 1951 0750.2 1991 0748.7 2008 0747.9 2045 0765.2
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 GR
 GR
         1880 0766.1 1835 0765.5 1814 0765.3 1783 0764.7 1752 0764.1
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 GR
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 N
         736.2 2 1
 PD
         740 2 2
 PD
 PD
         740 4 3
 PD
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         747 6 5
 PD
         3 110 2 758.3
 CD
       Completed Reading Data Associated With Header Record BRDGE
+++072 NOTICE: X-coordinate # 2 increased to eliminate vertical segment.
+++072 NOTICE: X-coordinate # 4 increased to eliminate vertical segment.
+++072 NOTICE: X-coordinate #24 increased to eliminate vertical segment.
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*** Storing Bridge Data In Temporary File As Record Number 3
***
                Data Summary For Bridge Record BRDGE
                                                              ***
                  150. Cross-Section Skew: .0 Error Code 0
SRD Location:
Valley Slope: ****** Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00
                   X,Y-coordinates (40 pairs)
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            765.900
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 1682.000
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 1628.000
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               Minimum and Maximum X, Y-coordinates
 Minimum X-Station: 1628.000 (associated Y-Elevation: 760.200)
 Maximum X-Station: 2049.100 (associated Y-Elevation: 765.700)
 Minimum Y-Elevation: 734.700 (associated X-Station: 1754.000)
 Maximum Y-Elevation: 766.400 (associated X-Station: 1942.000)
                  Roughness Data ( 1 SubAreas )
                         Roughness Horizontal
                SubArea Coefficient Breakpoint
                            .034
                        -----
                Discharge coefficient parameters
            BRType BRWdth EMBSS EMBElv UserCD
              3
                   110.000 2.00 758.300 *******
                    Pressure flow elevations
                      AVBCEL
                               PFElev
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                               760.000
                     Abutment Parameters
      ABSLPL ABSLPR XTOELT YTOELT
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                                         XTOERT
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Pier/Pile Data ( 5 Group(s) )
Code Indicates Bridge Uses Piers

	Group	Elevation	Gross Width	Number	
	1		2.000		
	2	740.000	2.000	2	
		740.000	4.000		
	4		4.000	4	
	5		6.000	5	
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COUNTY	: MARION		QUAD:	BEECH GROVE 12	4 B
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735					
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N	.100 .035				
SA	1695				
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SRD Locat			-Section Skew		Code 0
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Energy Lo	oss Coeffici	ents -> E	xpansion: .	50 Contraction	on: .00
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1230.000					
1706.000					
1769.000					
1862.000				1001.000	
		-			

```
Minimum and Maximum X, Y-coordinates
   Minimum X-Station: 968.000 (associated Y-Elevation: 760.000)
  Maximum X-Station: 1862.000 (associated Y-Elevation: 760.000)
   Minimum Y-Elevation: 734.500 (associated X-Station: 1730.000)
   Maximum Y-Elevation: 760.000 (associated X-Station:
                                            968.000 )
               Roughness Data ( 2 SubAreas )
                     Roughness Horizontal
              SubArea Coefficient Breakpoint
                       .100
                       - - -
                              1695.000
                       .035
              ......
Bridge datum projection(s): XREFLT XREFRT FDSTLT FDSTRT
                    ****** ***** *****
            Finished Processing Header Record APPR
        *----*
   Federal Highway Administration - U. S. Geological Survey
          Model for Water-Surface Profile Computations.
          Input Units: English / Output Units: English
   *----
      CARSON AVE OVER LICK CREEK AND I-465 I-465-165-4442
                             QUAD: BEECH GROVE 124 B
   COUNTY: MARION
      4-10-97
                                BRET A. ROBINSON
 EX
       Summary of Boundary Condition Information
       Reach Water Surface Friction
      Discharge
                Elevation Slope
                                     Flow Regime
               .....
       ------
        6980.00
                 *****
                            .0011
    1
                                      Sub-Critical
                 *****
    2
        9640.00
                            .0011
                                      Sub-Critical
       *-----
             Beginning 2 Profile Calculation(s)
       *====================================
   ******************* W S P R O ***************
     Federal Highway Administration - U. S. Geological Survey
          Model for Water-Surface Profile Computations.
          Input Units: English / Output Units: English
      CARSON AVE OVER LICK CREEK AND I-465 I-465-165-4442
```

COUNTY: MARION QUAD: BEECH GROVE 124 B 4-10-97 BRET A. ROBINSON

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: EXIT Header Type: XS SRD: .000	743.936 744.136 741.683	.200	6980.000 2.040 .309	3421.079 210347.30 *****	****** ****** 3.092	1007.946 1823.777 *****
Section: FULLV Header Type: FV SRD: 150.000	744.114	.182	6980.000	3565.926	150.000	1005.872
	744.296	.156	1.957	222779.70	150.000	1824.397
	741.683	.000	.289	.0010	3.057	.003

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "APPR ". KRATIO: .63

Section: APPR	744.219	.779	6980.000	1639.642	260.000	1299.477
Header Type: AS	744.998	.408	4.257	139490.40	260.000	1801.110
SRD: 410.000	742.361	.298	.690	.0016	2.763	003

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

<<< The Following Data Reflect The "Constricted" Profile >>>
 << Beginning Bridge/Culvert Hydraulic Computations >>>

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	НО	FR #	SF	ALPHA	ERR
Section: BRDGE	743.908	1.028	6980.000	858.571	150.000	1663.340
Header Type: BR	744.936	.288	8.130		150.000	1802.417
SRD: 150.000	741.953	.511	.577	****	1.000	.000
Specific Bridge					XLAB	XRAB
Bridge Type 3 Pier/Pile Code				.000 *****		
	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	v	K	FLEN	REW
	CRWS	НО	FR #	SF	ALPHA	ERR
Section: APPR	745.249	.489	6980.000	2201.344	150.000	1224.231
Header Type: AS	745.738	.344	3.171	185162.10	157.859	1801.624
SRD: 410.000	742.361	.457	.506	.0016	3.130	007

Approach Section APPR Flow Contraction Information M(G) M(K) KQ XLKQ XRKQ OTEL

.721	.161	155692.4	1661.407	1800.483	745.249

<<< End of Bridge Hydraulics Computations >>>

Federal Highway Administration - U. S. Geological Survey Model for Water-Surface Profile Computations.

Input Units: English / Output Units: English

CARSON AVE OVER LICK CREEK AND I-465 I-465-165-4442
COUNTY: MARION QUAD: BEECH GROVE 124 B
4-10-97 BRET A. ROBINSON

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	НО	FR #	SF	ALPHA	ERR
Section: EXIT	745.011	.226	9640.000	4306.739	*****	995.370
Header Type: XS	745.237	****	2.238	290533.90	*****	1827.539
SRD: .000	742.229	*****	.295	*****	2.899	****
Section: FULLV	745.186	.209	9640.000	4452.751	150.000	993.321
Header Type: FV	745.396	.157	2.165	304672.70	150.000	1828.152
SRD: 150.000	742.229	.000	.280	.0010	2.872	.001

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "APPR ". KRATIO: .61

Section: APPR	745.247	.934	9640.000	2200.353	260.000	1224.271
Header Type: AS	746.181	.428	4.381	185074.00	260.000	1801.624
SRD: 410.000	743.494	.362	.700	.0016	3.129	005

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

<<< The Following Data Reflect The "Constricted" Profile >>>
 <<< Beginning Bridge/Culvert Hydraulic Computations >>>

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: BRDGE	744.877	1.494	9640.000	995.257	150.000	1661.296
Header Type: BR	746.372	.318	9.686	155358.80	150.000	1804.167
SRD: 150.000	743.087	.818	.655	*****	1.024	.001
	Information Flow Type 1 0			LEV BLEN .000 ******	XLAB  * ******	XRAB  * *******

	EGEL CRWS	HF HO		AREA K SF		REW ERR
Section: APPR Header Type: AS SRD: 410.000	746.795 747.279	.484 .364	9640.000	3122.325 272169.80	150.000 161.21	1188.364
	oroach Section () M(K)	KQ	XLKQ	XRKQ	OTEL	
	750 .225	211294	.8 1656.9	35 1799.80	2 746.79	
<	<pre>:&lt;&lt; End of Br</pre>	idge Hyd	raulics C	omputation	s >>>	
Federal H Mo Inp	*************  ighway Admin  del for Wate  out Units: En	istratio r-Surfac glish /	n - U. e Profile Output	S. Geologio Computatio Units: Eng	cal Survey ons. lish	7
	AVE OVER LICK	CREEK A	ND I-465 QUAD		-4442 VE 124 B	*
*** Live-Bed C			culations nput Vari		Record E	BRDGE ***
Bed Tot	. Material Tr al Pier Widt	ansport 1 h Value	Mode Fact	or (k1): (Pw):	.64 5.000	
Scour # Depth Contr	act Approach	Contra	ct Approa	ch Side	Contract	Approach
1 2.632 6236 Approac 2 4.173 8234 Approac	790 5038.52 h Channe1 De 653 6084.82 h Channel De	6 68.0 pth: 9 68.0 pth: 1	00 75.0 9.512 00 75.0 1.058	00 Left: Right: 00 Left: Right:	1692.000 1766.000 1692.000 1766.000	1695.000 1770.000 1695.000 1770.000
Mo Inp	************ ighway Admin del for Wate ut Units: En	istratio r-Surfac glish /	n - U. e Profile Output	S. Geologia Computatia Units: Engl	cal Survey ons. Lish	,
	AVE OVER LICK		ND I-465 QUAD:		4442 VE 124 B	*

\*\*\* Pier Scour Calculations for Header Record BRDGE \*\*\*

Constants and Input Variables

Pier Width: 2.000									
		Pier S Flow A Bed Co Bed Ma Veloci Depth	Shape Fac angle of ondition terial F ty Multi Multipli	tor Attack : Factor actor plier er	Factor	(K1): (K2): (K3): (K4): (VM): (YM):	1.0 1.1 1.0 1.0	00 00 00 00 00	
#	Depth	Loca Flow	WSE	Depth	Velocit	y Fro	ude #	Left	Right
1	5.79 6.31	6980.000 9640.000	744.364 745.419	9.664 10.719	9.272 10.956	2 5	.526 .590	1628.000 1628.000	2049.000 2049.000
	CA:	Input Un RSON AVE OV MARION 0-97 Pier Sco	PER LICK	lish / CREEK AN	Output Output OU I-465 QUA	Unit	s: Eng 65-165 ECH GRO A. RO	lish	
				Width:			_		
		Pier S Flow A Bed Co Bed Ma Veloci Depth	hape Fac ngle of ndition terial F ty Multi Multipli	tor Attack I Factor actor plier er	Factor	(K1): (K2): (K3):	1.0 1.0 1.1	0 0 0 0	
#	Scour Depth	Loca Flow	lized Hy WSE		Propert Velocit			X-Sta Left	tions Right
1 2	5.79	6980.000 9640.000			9.272		.526	1628.000	2049.000
EF	ξ ******	****	Normal	end of V	VSPRO ex	ecutio	on. *	*****	****